



A comprehensive biofiltration model
and its calibration and validation
for a large-scale nitrifying WRRF under upgrade

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 - Upgrade of the Seine Aval WRRF
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- Aims of the modelling work
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 - Results and discussions
- Conclusions

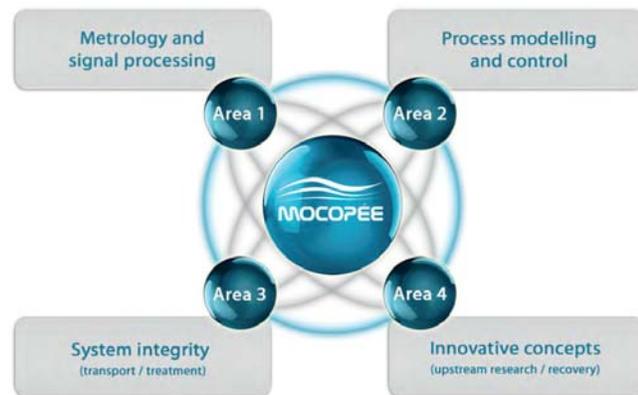
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Modelling, control and optimization of wastewater treatment processes

- Research program launched in 2014
2nd five-year phase started in 2018
- About the program
 - Four applied research axes
 - Budget 1-2 M€/yr
 - Around 30 research teams involved
 - 11 PhD students since 2014
- Supported by the Greater Paris Sanitation Authority (France)



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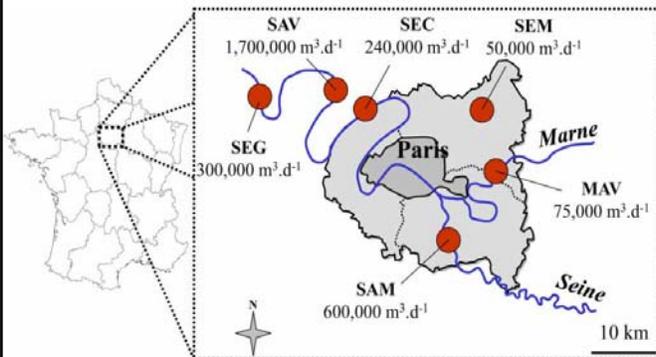


Figure 2: SIAAP's water resource recovery facilities.

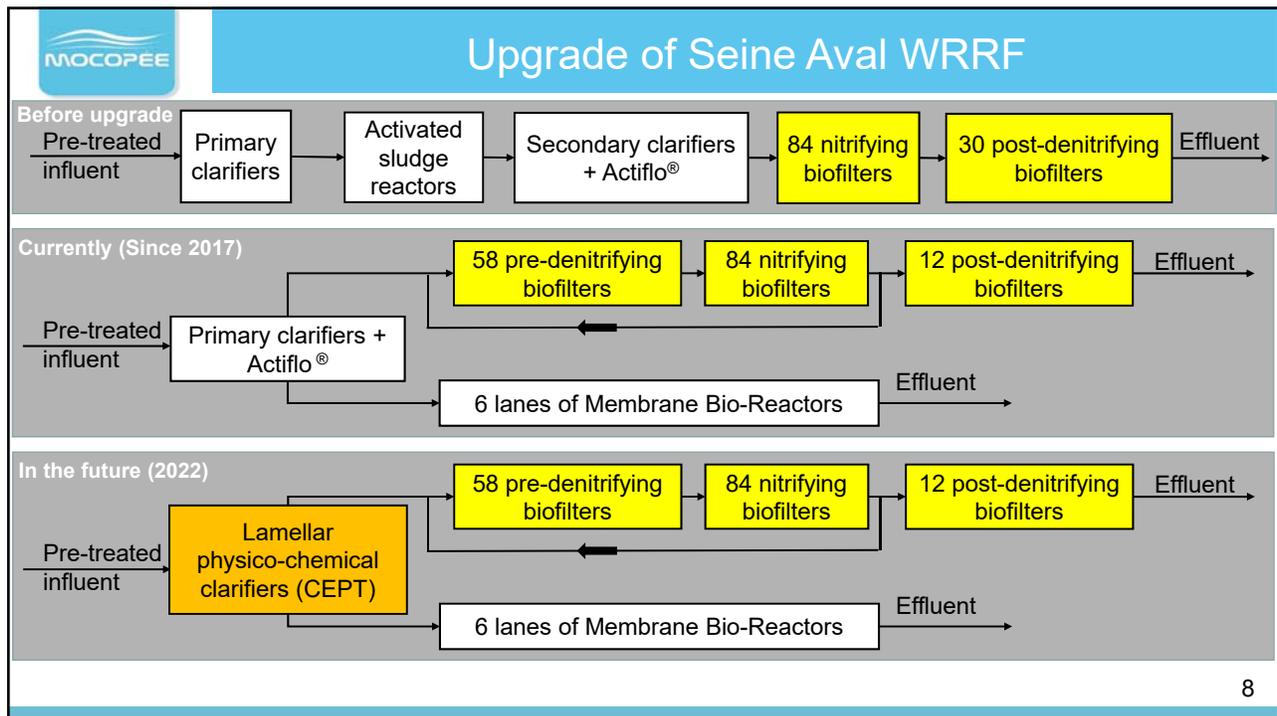
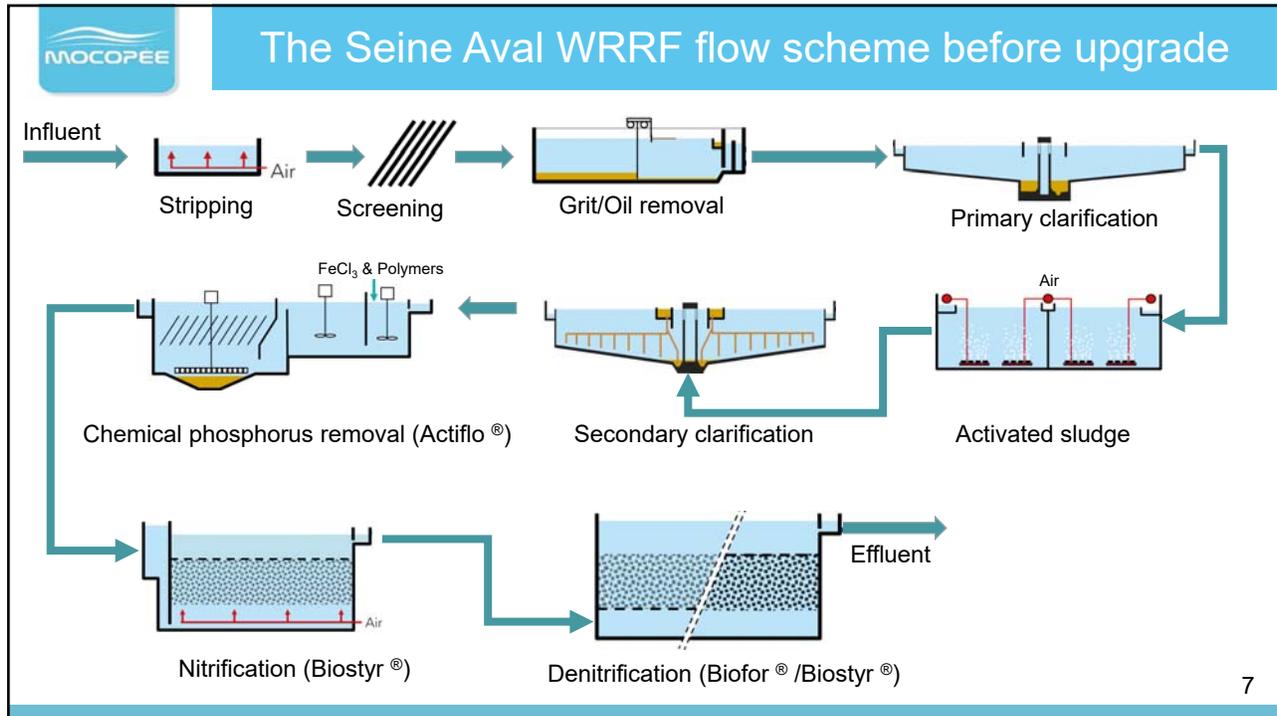
- 6 water resource recovery facilities in the Paris region
- 2,5 million m³ of wastewater treated each day
- 9 million inhabitants



Figure 3: Seine Aval (SAV) WRRF

- Nominal flow designed : 1,7 million m³/d
- 5 million inhabitants

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MACOPEE Nitrification → Biostyr®

The diagram illustrates the Biostyr nitrification process. Influent enters from the left, and effluent exits from the right. Air is injected from the bottom through a series of nozzles. The support media (Biostyr) is located in the center. The floor of the tank is shown at two levels. Below the diagram are three petri dishes showing the media at different stages of biofilm growth: brown, tan, and white. To the right are two test tubes showing the media with biofilm.

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MACOPEE Nitrification → Biostyr®

Filtration

Treated water

Wastewater with large particles

Backwash

Washing water flux

Detached biofilm

Biofilter in BIOSTYR® type

Labels: nozzle deck, influent channel, air, EFFLUENT, INFLUENT, to effluent channel

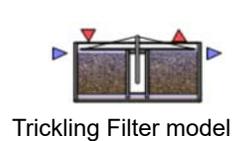
BIOSTYRE™ media bed

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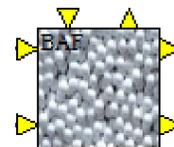
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1. Develop models for each treatment process, simulate their performances and evaluate economic and environmental impacts.
2. Develop and use models as decision support tools for the distribution of the influent between the different processes.
3. Develop and use models for process control and optimization.



Trickling Filter model



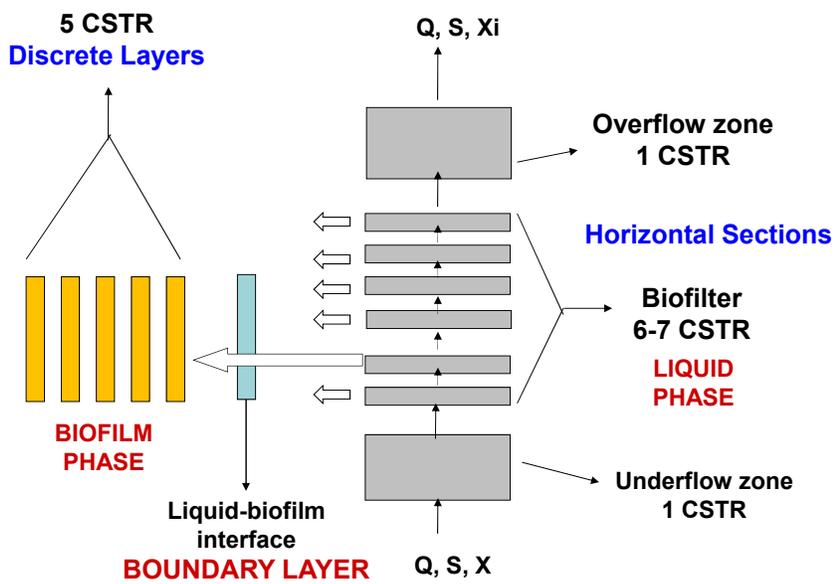
Submerged biofilter model

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- Vigne et al. (2010)
- GPS-X



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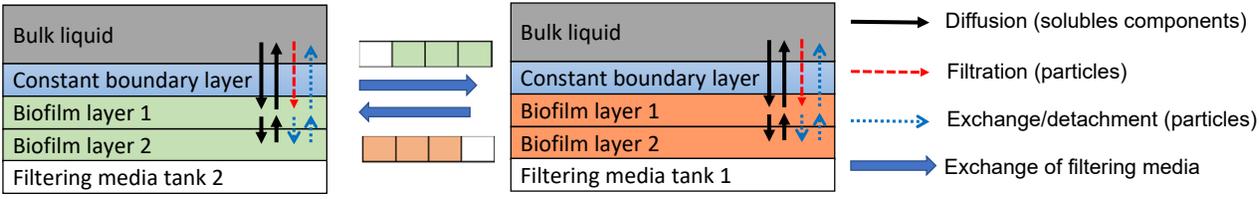


Model development work on Biofiltration stage

Model description I – Original model (Bernier et al., 2014)

1. 6-7 reactor tanks-in-series (vertical tanks, each 0.5 m of media bed)
2. 4 principal submodels : biofilter hydraulics, mass transport, 2-layer biofilm model and biological reactions.
3. Mass transport : diffusion, filtration, exchange and detachment
4. Biological reactions : Modified ASM1 (2-step nitrification/denitrification)
5. Backwash process (1/day) with media exchange between vertical tanks



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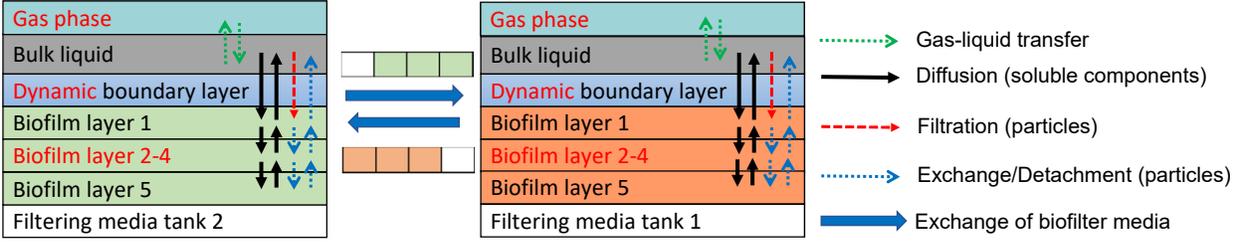


Model development work on Biofiltration stage

Model description II – Model modifications (Mass transport)

1. Boundary layer with variable thickness (fluid and media properties)
2. More biofilm layers are considered (5 layers).
3. A gas phase and gas liquid transfer are introduced
4. Modification of particles mass transport
5. Improved media exchange between media tanks (to maintain biomass spatial organization)

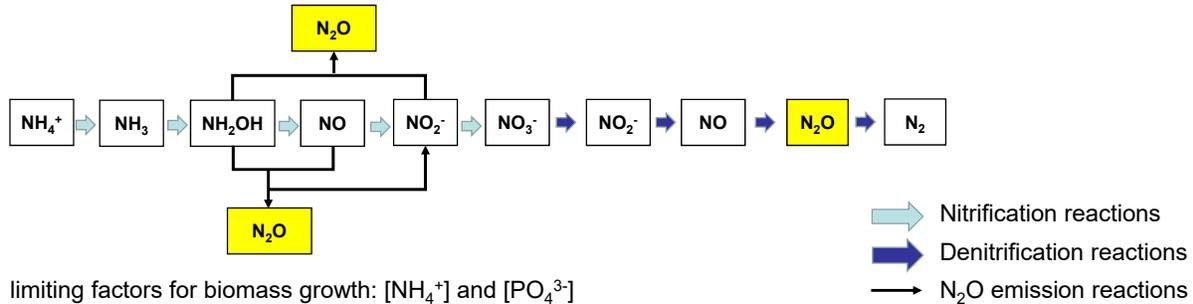




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Model description III – Model modification (Biological reactions and energy consumption)

Nitrification and denitrification in the modified model (Hiatt & Grady, 2008, Pocquet et al., 2016)



 **Pumping energy evaluation** (According to Gernaey et al., 2006)

 **Aeration energy evaluation** (According to Wu et al., 2005)

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Model description IV – Model modification (Energy consumption)

Aeration energy estimation (according to Wu et al., 2005)

$$E_{aeration} = 0.024 \int \frac{Q_{air} * \Delta P}{\eta}$$

- Q_{air} is the air flow delivered by compressors to the stage (m^3/d)
- ΔP is the differential pressure (Pa)
- η is the overall efficiency of the compressors (-)

Pumping energy estimation (according to Gernaey et al., 2006)

$$E_{pomp} = n * 0.024 \int \frac{(K' * Q_{fluid}^2 + H_{geo}) * Q_{fluid} * g * \rho}{\eta}$$

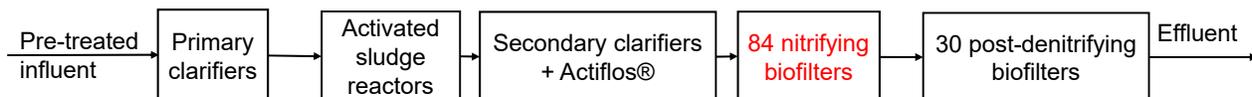
- n is the number of active pumps
- K' is the coefficient covering the friction headloss, minor losses and velocity head (d^2/m^5)
- H_{geo} is the geometric height (m) of the pump
- Q_{fluid} is the bulk liquid flow delivered by the pump (m^3/d)
- g is the gravity acceleration (m/s^2)
- ρ is the density of the fluid (kg/m^3)
- η is the overall efficiency of the pump

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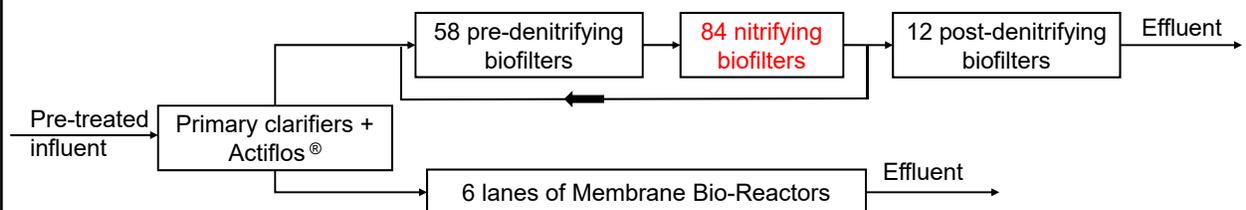
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Configuration before upgrade (for calibration)



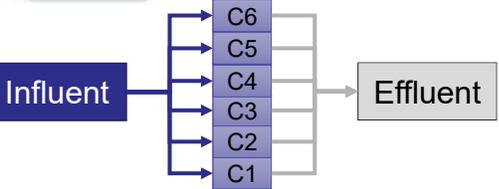
Current configuration (Since 2017, for validation)



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Calibration and validation of the nitrifying stage



C1 = 1 treatment cell (contains 14 biofilters)
Media bed height = 3,5 m

Daily average monitoring data	Sampler location
NO_3^-	Influent
TKN	Influent
Alkalinity	Influent
COD	Influent/Effluent
NO_2^-	Influent/Effluent
filtered COD*	Influent/Effluent
TSS	Influent/Effluent
NH_4^+	Influent/Effluent

* Filtered COD was only available in 2017

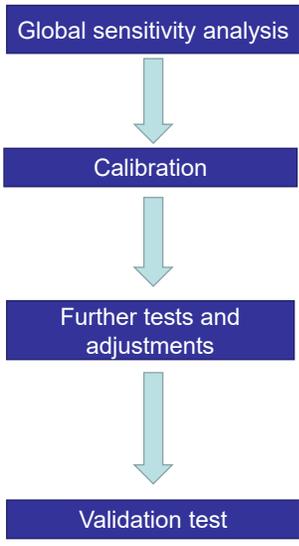
Sensor data (each 15 min)	Sensor location
Water flow rate	Influent
Air flow rate	Influent
TSS	Influent
PO_4^{3-}	Influent
Temperature	Influent
NH_4^+	Influent/Effluent
NO_3^-	Effluent
DO	Effluent

Operational information: Aeration and pumping energy

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Calibration and validation of the nitrifying biofilter model

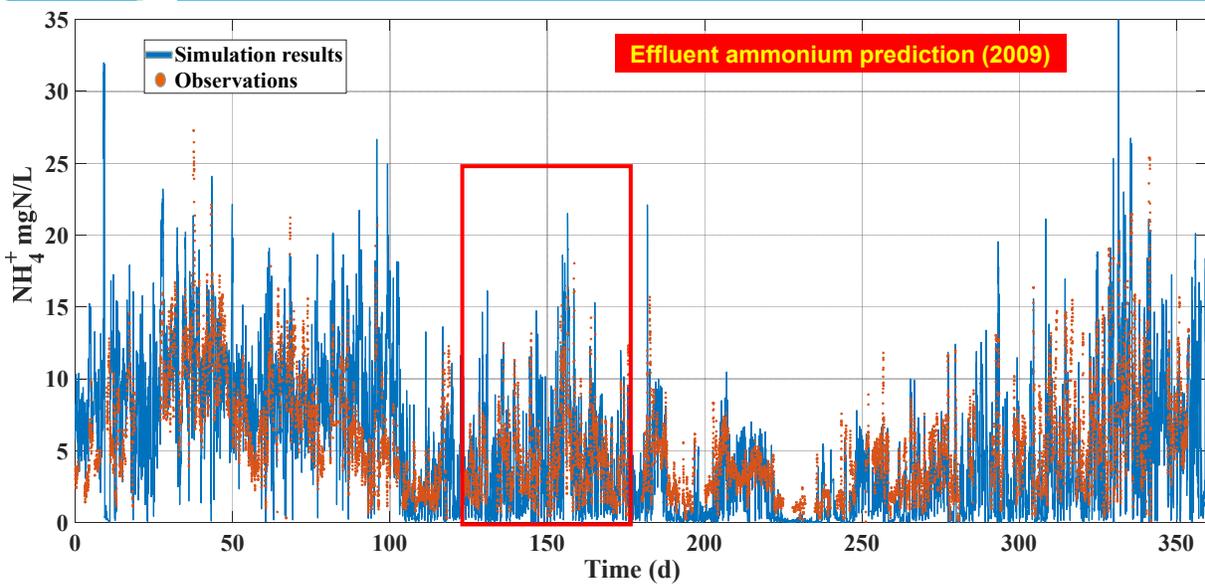


- To identify influential parameters
- To reduce the number of parameters to be calibrated
⇒ Monte-Carlo approach for sensitivity analysis (Sin et al., 2011)
- To identify the best parameter values
⇒ Monte-Carlo approach for calibration (Sin et al., 2008)
⇒ 30 days of data over summer holiday (2009)
⇒ Pollution load decreased in this period
- To test and improve model prediction performance for long term period
⇒ Test 1: 60 days of data after summer holiday (2009)
⇒ Test 2: Entire year of data for 2009
⇒ Manual adjustments for a few parameter values
- To validate model performance under current treatment configuration
⇒ 180 days of data for year 2017
⇒ Only one aeration parameter value had to be changed (aging of aerators)

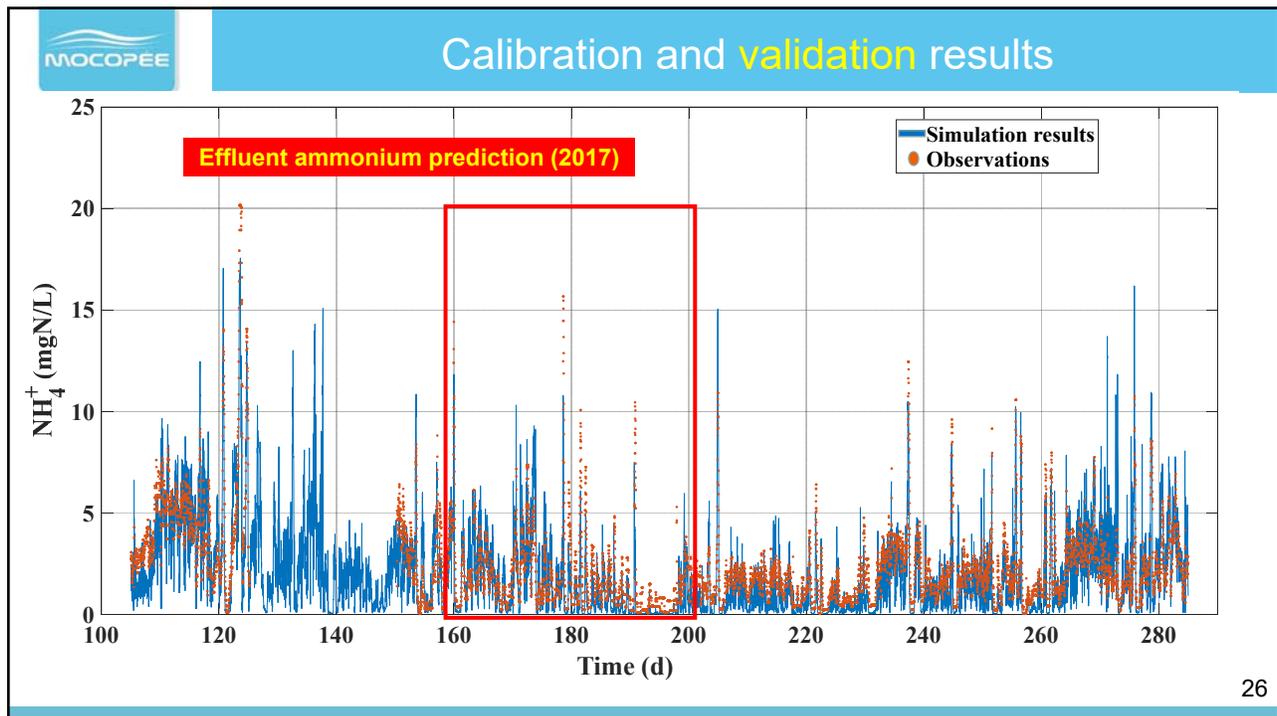
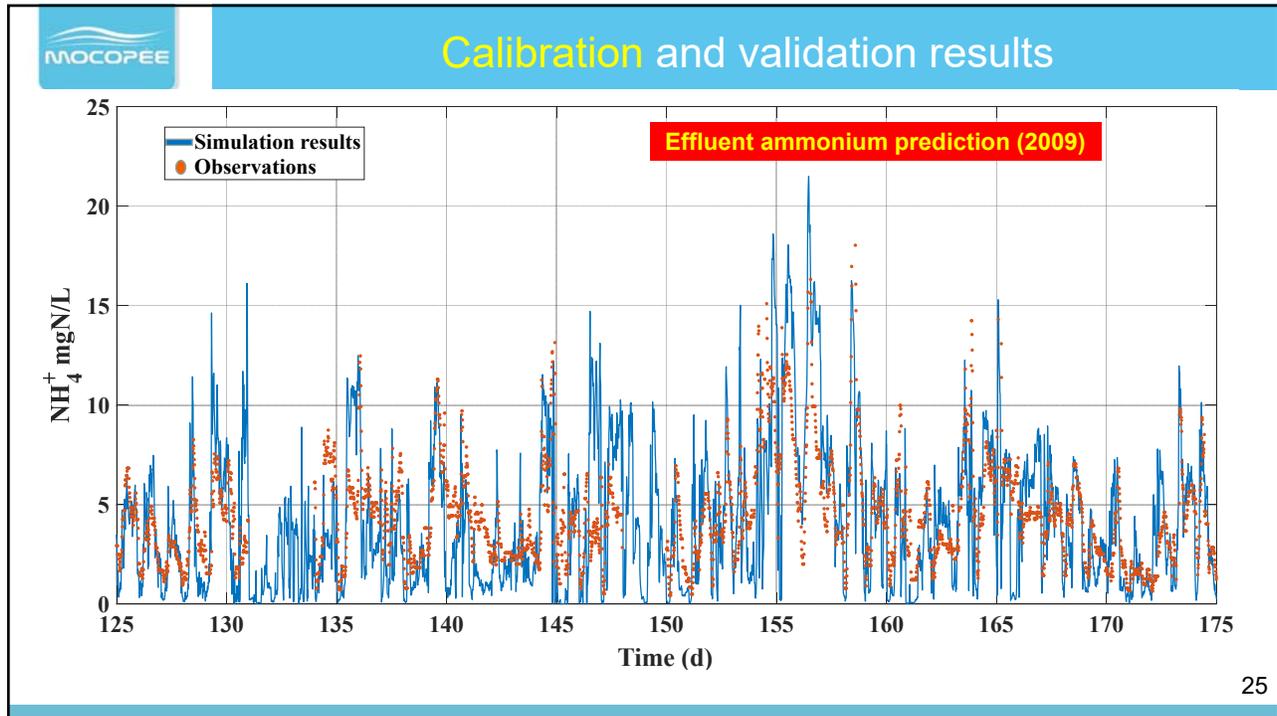
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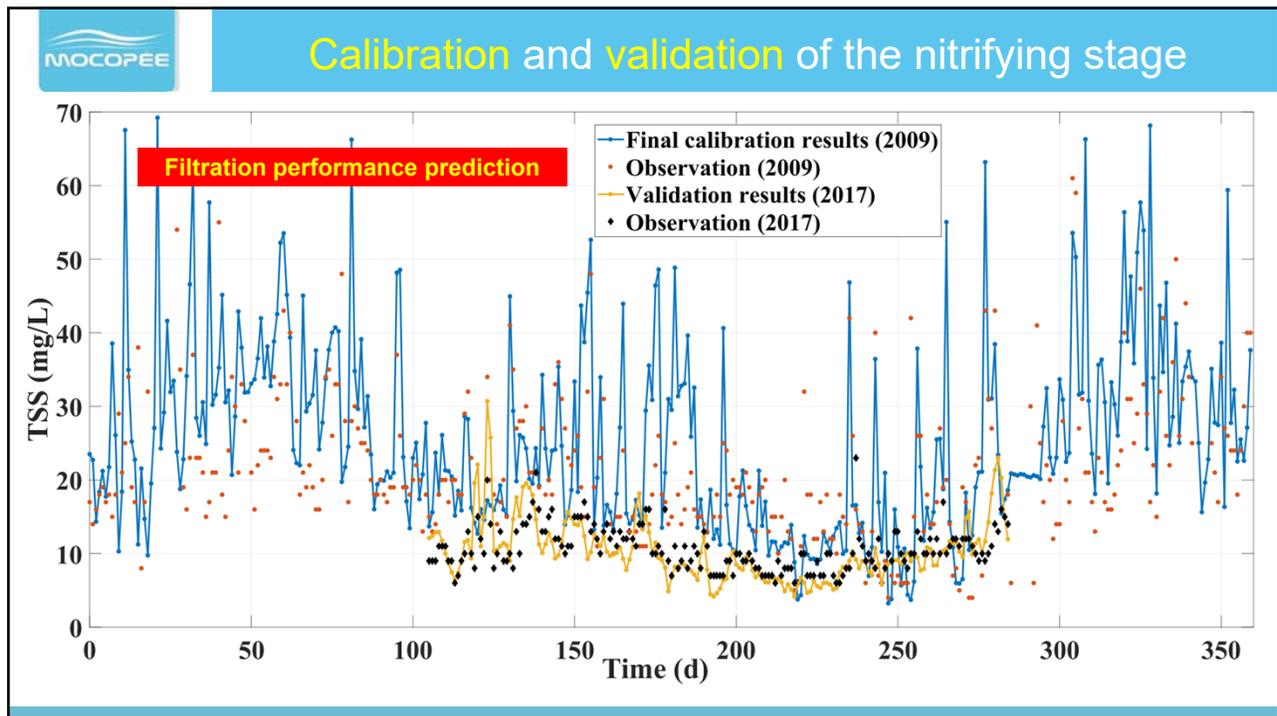
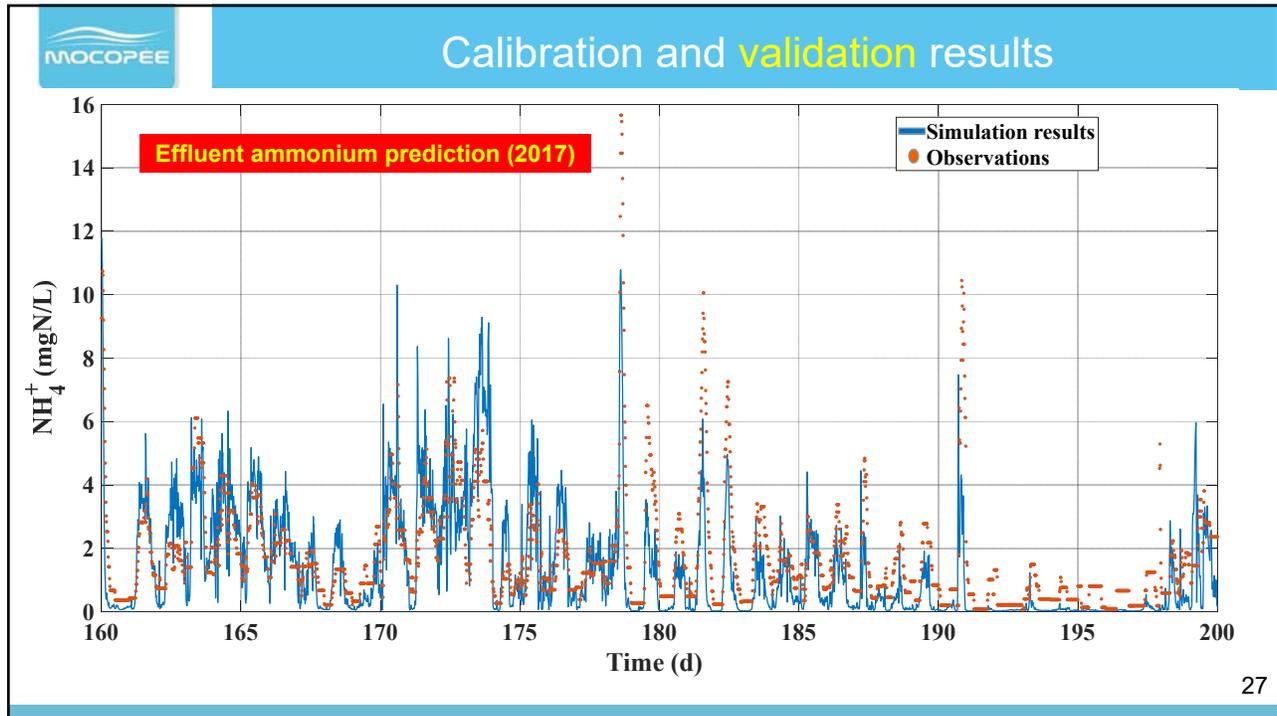
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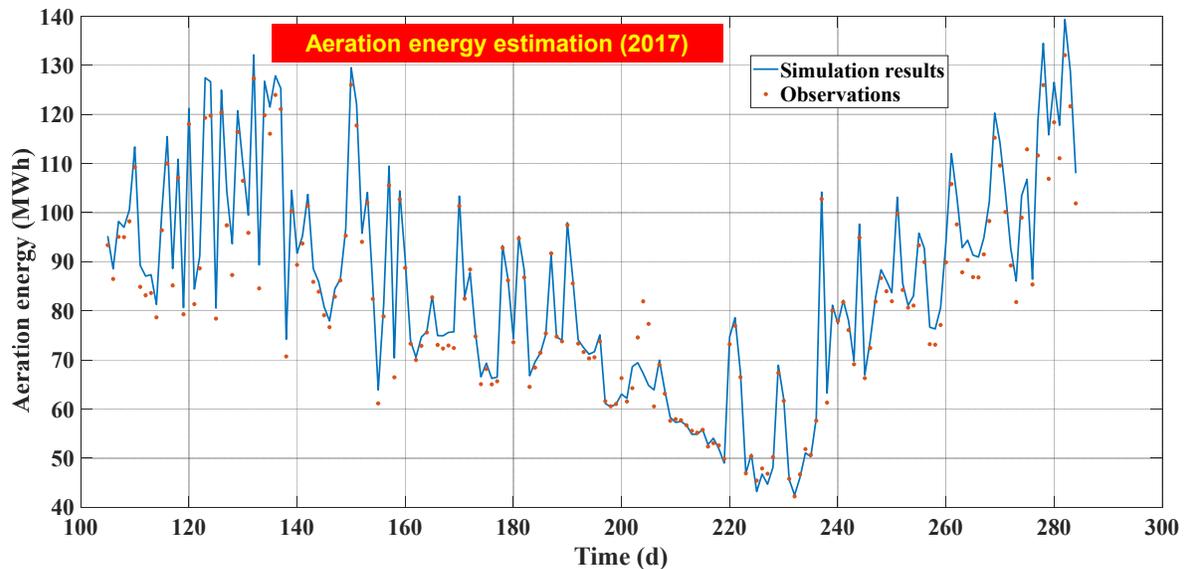


Summary of statistical scores

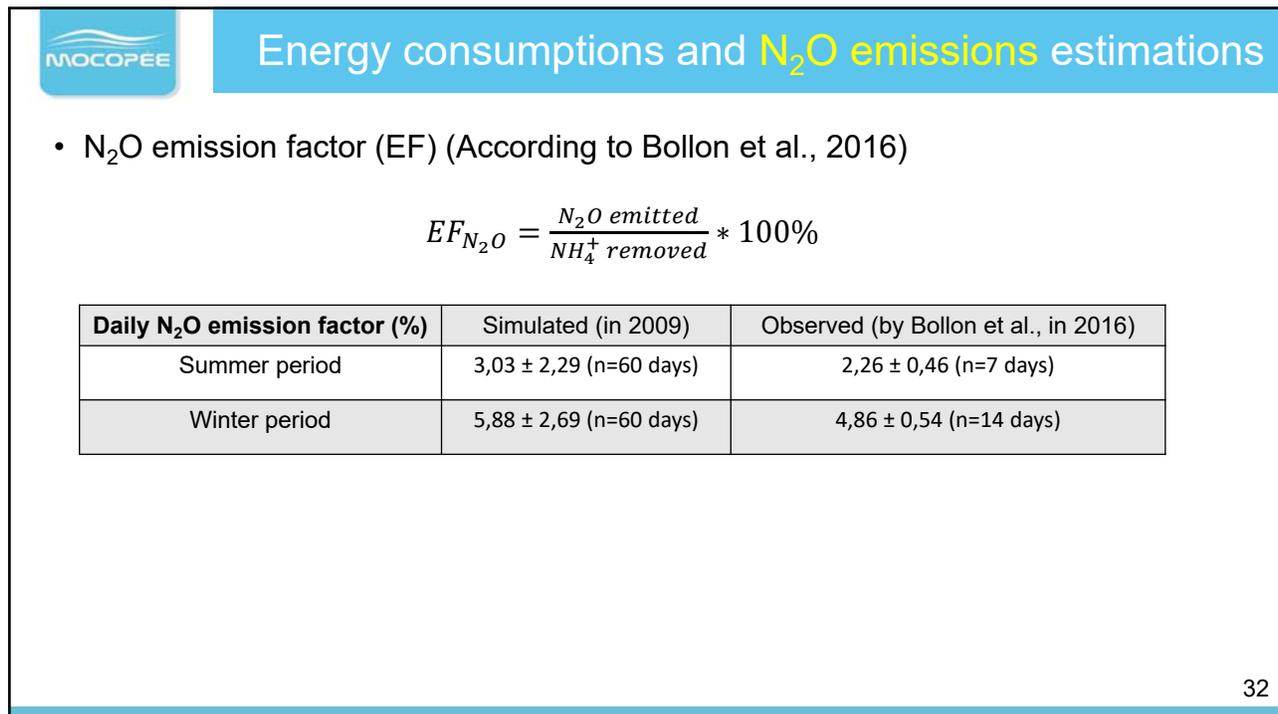
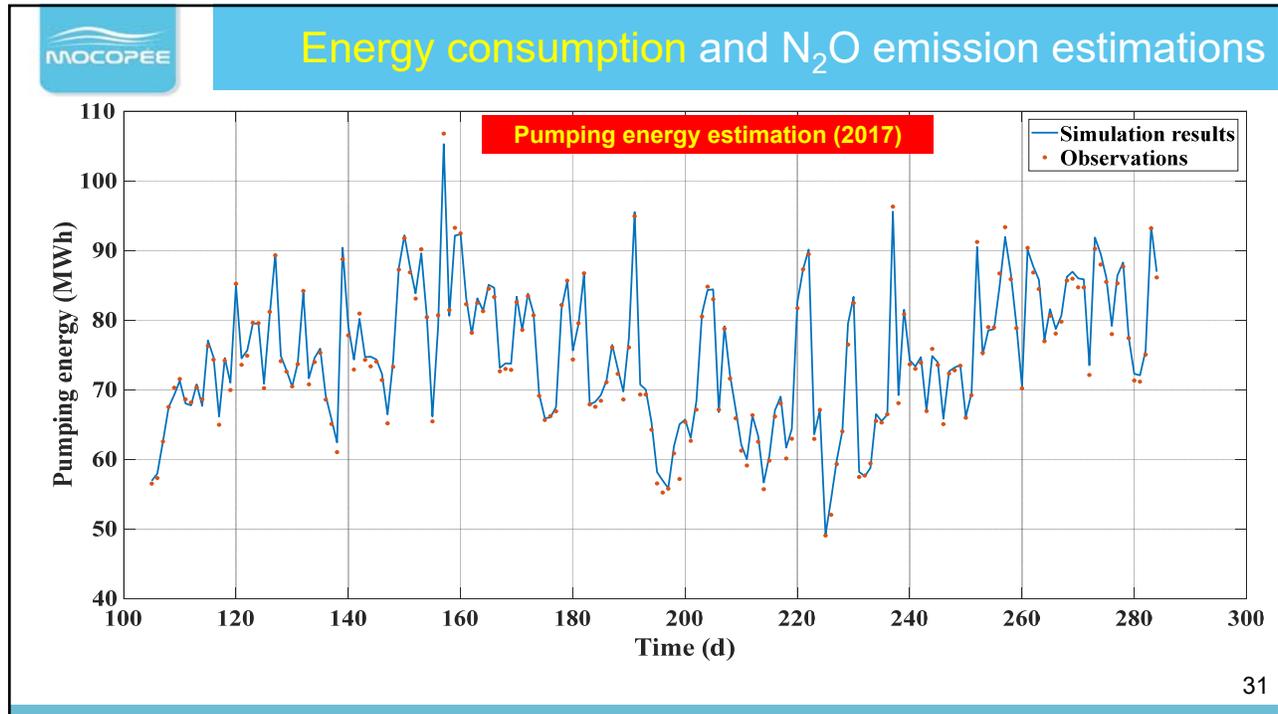
Scores for 2009 (calibration)	NH ₄ ⁺	NO ₃ ⁻	DO	NO ₂ ⁻	COD	TSS	PO ₄ ³⁻
Number of validated observations (n)	27048	34272	33313	329	331	332	329
Observed mean (mg/L)	5.55	34.04	6.63	0.78	62.27	21.58	0.39
Mean error (ME) (mg/L)	-0,32	2,19	-0,22	-0,13	-2,99	3,87	0,07
Root mean square error (RMSE) (mg/L)	3,58	4,55	0,79	0,56	15,08	11,83	0,16

Scores for 2017 (validation)	NH ₄ ⁺	NO ₃ ⁻	DO	NO ₂ ⁻	COD	TSS	PO ₄ ³⁻
Number of validated observations (n)	14841	14841	17226	178	180	180	180
Observed mean (mg/L)	2.30	19.12	6.40	0.77	41.52	10.68	0.76
Mean error (ME) (mg/L)	-0,33	1,35	-0,92	0,16	-0,52	-0,32	-0,12
Root mean square error (RMSE) (mg/L)	1,53	3,13	1,26	0,78	5,44	3,39	0,17

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- Modified multi-layer ASM1GHG biofilm model
 - N-species (NO₂)
 - Mass transport: Filtration, detachment, exchange of biofilm
 - Energy consumptions (aeration, pumping)
 - N₂O emissions
- Calibration and validation for the nitrifying stage (Biostyr®)
 - 2009, 2017 configurations
 - Good prediction performances
- Project progress and perspectives
 - Modelling of post-denitrification and CEPT (finished)
 - Modelling of pre-denitrification (in progress)

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